

Population models of turbulent heat and mass transfer by Brian Spalding, CHAM Ltd

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Summary

Conventional turbulence models handle only macro-mixing.

They calculate the **time-mean** concentrations in plumes, arriving at skimpy, reality-missing results *e.g.* for the '**profile**' across the plume like this->



Population models of turbulence handle micro-mixing in addition.

They are **needed** for **realistic** prediction of **non-linear** processes such as: * thermal **radiation**, * chemical **reaction**, * **biological** response,

* fluid-structure interaction, * condensation and evaporation, * etcetera.

Population models of turbulence predict probability-density functions.

They **discretize** these **pdf**s. Then they treat the histogram ordinates as dependent

variables of individual conservation equations .



They also allow **population-grid refinement'.**



Population models of turbulent heat and mass transfer; how turbulent mixing proceeds

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Boussinesq's enlarged-viscosity concept predicts macro-mixing well, but not micro-mixing. It is eddy roll-up, enlarging interface areas and concentration gradients, which allows laminar diffusion to do its work.



On the left is Urban Svenson's 1998 numerical simulation of the **Kelvin-Hemholtz** instability which causes eddy roll-

The probability-density function for this location will look like this:



ity-density function of concer

On the right is a sketch of the 1970's **'ESCIMO'** concept of how **'Engulfment'** and **'Stretching' increase gradients** of temperature and concentration and so facilitate chemical reaction (Noseir, 1980).





Population models of turbulent heat and mass transfer; fundamental concepts

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- In what follows, **transient engulfment** and **stretching** processes are postulated as occurring **continually and throughout** the turbulent fluid.
- They can be likened to 'brief encounters' between unlike parents, leading to offspring of intermediate complexion, as illustrated here:



- In the absence of other guidance, the **rate of offspring production** is taken as proportional to the **parent-concentration product**, times: *the square root of the sum of products of velocity gradients.*
- This square root, multiplied by the effective viscosity, represents the generation rate of turbulent kinetic energy,

linking conveniently with hydrodynamic turbulence models e.g. k-epsilon.

• The **pdf**'s (now also called **population distribution functions**) of **complexion** are then computed *via* simple **mass balances**.



Population models of turbulent heat and mass transfer; some history

- The use of mass-balance (*I.e.* 'pdf-transport') equations for computing population distributions was proposed by **Dopazo** in 1975.
- Numerical solutions were first provided in 1981 by **Pope**, who (wisely?) chose the **Monte-Carlo** method for doing so.
- •Computations by **Fueyo** (2008) for hydrocarbon combustion, shown here, were also obtained by the Monte-Carlo method.



Figure 7. Instantaneous flame structure. Top: isocontours of OH in LES calculation; middle: isocontours of reaction rate in LEM calculation; bottom: isosurface of stoichiometric mixture

- In 1996, independently and as a generalisation of the 1971 'eddybreak-up' concept, I created the 'multi-fluid model'. This discretized the pdf, treating the histogram ordinates as the dependent variables of a sufficient number of differential equations.
- Both **1D**

and 2D

- histograms were used;
- and attention was given to **how many** distinct 'fluids' (*I.e.* histogram ordinates) were required for for accuracy.
- This **population-grid-refinement** possibility, not available in the Monte Carlo method, is an advantage of the discretized approach.



Population models of turbulent heat and mass transfer; **questions** which **research** could answer.

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- 1. The **'offspring-production-rate' equation** contains a proportionality constant (**CONMIX** below) which must be obtained from **experiment**.
- What is its **value**?
- Is it indeed a constant?
- If not, does it depend on Reynolds Number? on energydissipation/production-rate ratio? on something else?
- 2. Are 'complexions' of the offspring **distributed** In uniform '**Mendelian**' fashion shown on the right)?





Or is there just one offspring complexion, as shown on the left?

3. Pdf's of temperature are **easy to measure**; and their **shapes** depend on the assumptions made for CONMIX and offspring distributions. Therefore the research questions can be answered, by **comparing** with experimental contour and pdf shapes and sizes (see next slides).

4. Unfortunately few researchers practise **both** experimental and numerical studies. How to change **that** is the **most pressing research challenge.**



Population models of turbulent heat and mass transfer;

numerical solutions of the conservation equations

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Results will be presented for the much-studied steady axi-symmetrical uniform-density turbulent jet.

The **macro-mixing** part of the model is **conventional** in that:

• the **k-epsilon model** is employed for the calculation of the **effective viscosity**; and

• a constant **effective Prandtl number** characterises the turbulent diffusion of each of the hypothetically distinct fluids.

The **micro-mixing** part of the model is **unconventional**, in that: • each equation has a **source term** which expresses its rate of creation by the evening out of the steep concentration gradients within the engulfed eddy; and

• it has a corresponding **sink term** expressing its contributions, with partnering 'parents', to new engulfments.

If this mingling of disparate elements is adjudged inconsistent, so be it. Consistency is not always a virtue.



Population models of turbulence; fluid-concentration contours for a **steady axi-symmetrical jet** with CONMIX=100

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Numerical simulation with a **20-fluid model** and a 20*100 spatial grid leads to concentration contours of each fluid. *e.a.*:

1. Sum of all 20 fluids, *l.e.* the conventional mixture fraction

2. Fluid 1, of highest injectedsubstance concentration

3. Fluid 10, of smaller injectedsubstance concentration

4. Fluid 15, of still smaller injectedsubstance concentration

5. Fluid 20, of smallest injectedsubstance concentration







Note that 20 additional differential equations had to be solved!



Population models of turbulence; fluid-concentration contours for the jet, with **CONMIX=1 and 100 compared**

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With CONMIX=1 (on the left) the contours are **much broader** than with CONMIX=100 (on the right, as just seen). Which are the **more realistic**?

The '**true**' value of CONMIX can be established by **comparison** of experimentally-measure **pdf's** with calculated ones (see next slide).







Population models of turbulence; pdf's at two points on the jet axis, for CONMIX=1, 10 and 100



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Axial distance nozzle diameter = 10

Axial distance nozzle diameter = 18

Such large shape differences should make it easy to determine CONMIX



Population models of turbulent heat and mass transfer; population-grid-refinement effects

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Perhaps the 20-fluid model gives **insufficient resolution** of the pdf; therefore it is instructive to **vary the 'population-grid' fineness**, as shown below, for CONMIX= 5, for a point on the axis far from the nozzle.





Population models of turbulent heat and mass transfer; comments on the foregoing results

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1. Increasing the number of fluids does give the **expected smoothing** of the pdf shape; and it of course increases the computer time also.

2. Computer times are however very **small** (less than 1 PC minute).

3. The program was PHOENICS, which has a **built-in** (but useradjustable) **multi-fluid model** and a library of input files.

4. What is now needed is that **experimental researchers** should **use it**, or some equivalent software.

5. It is also desirable that **Direct Numerical Simulation** (DNS) practitioners should **post-process their results in terms of pdf's** and of the quantitative conditions which influence them.

6. Aiding turbulence modellers in this way may be regarded as **the main useful result** which can emerge from DNS studies, until computing power increases greatly.

7. But the modellers need to **abandon conventional Kolmogorov-type** models and **"think pdf".**



Population models of turbulent heat and mass transfer; three **practical reasons** for **computing pdf's** Rome, Italy Sept 14-18, 2009

1. Death can be caused by breathing **occasional whiffs** of high-concentration poison-gas, the **time-average** concentration of which may be **non-lethal**.





2. It is the occasional **high-velocity gust** which damages the wind turbine, **not the time-average** wind force.

3. **Explosions** can still occur when **only some** pockets of mixture are **in the flammable range** of air-fuel ratios, even though the mixture as a whole is **too rich** or **too lean** to burn.

It is differences from the mean which count !





Population models of turbulent heat and mass transfer; final remarks

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Four common misconceptions have been challenged, namely:

1. That turbulence models **must be** of **Kolmogorov** type, concerned only with **mixture-average** quantities, *e.g.* k, epsilon, RMS fluctuations, *etc.*, perhaps with **presumed pdf shapes.**

In fact, the pdfs of any fluid attribute (or pair of attributes) can be computed directly, with few and **testable** assumptions.

2. That Monte-Carlo methods **must be** used for computing pdfs.

In fact, **discretization** is simpler (to understand and to program), and more informative; moreover it allows population-grid refinement studies.

3. That CFD has at most 4 dimensions (3 of space and 1 of time).

In fact, it must become **multi-dimensional** if the **population-related** aspects of fluids are to be simulated

4. That turbulence modelling is a **unique activity**, unlike any other.

In fact, it is just one branch of **population modelling**, of which other branches concern: particle-size variation, bacterial growth and decay, animal-species interaction, *etcetera*.



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Thank you for your attention!



The End