



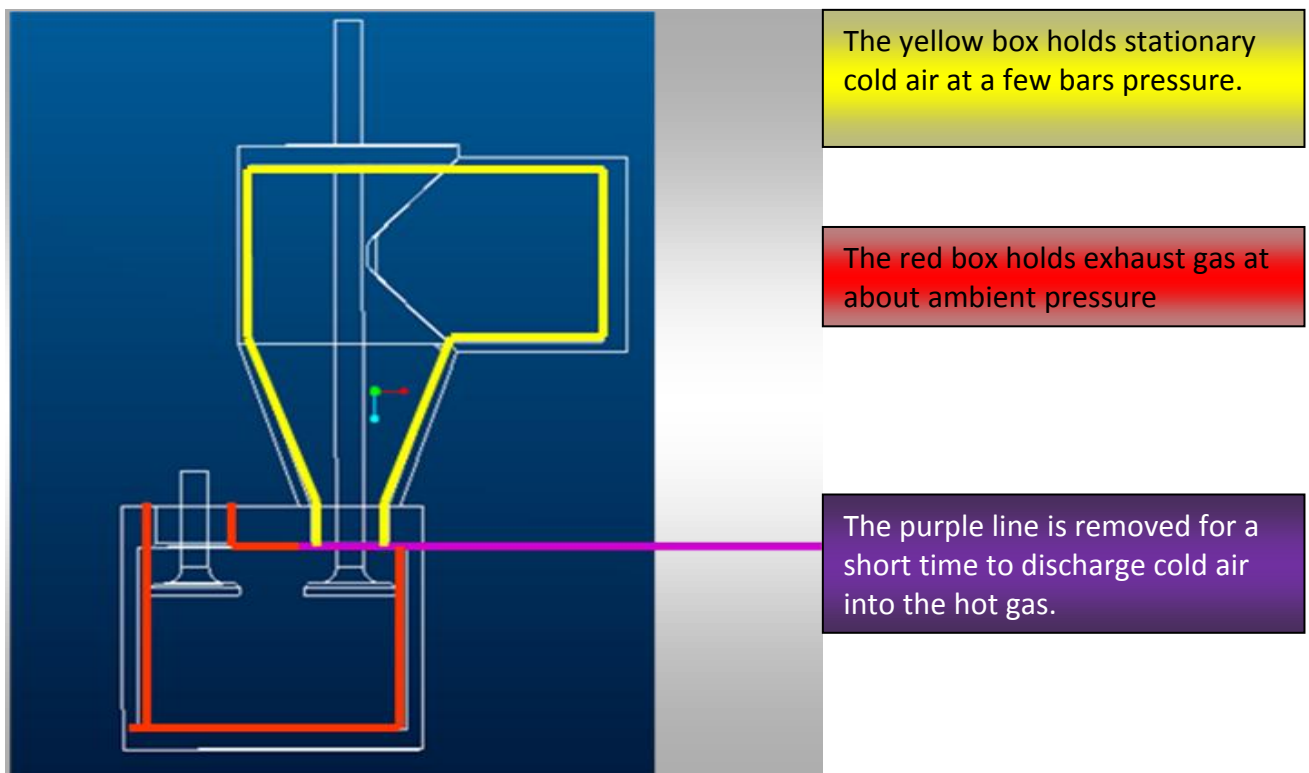
CHAM Limited
Pioneering CFD Software for Education & Industry

CHAM Case Study – Air Injector Model

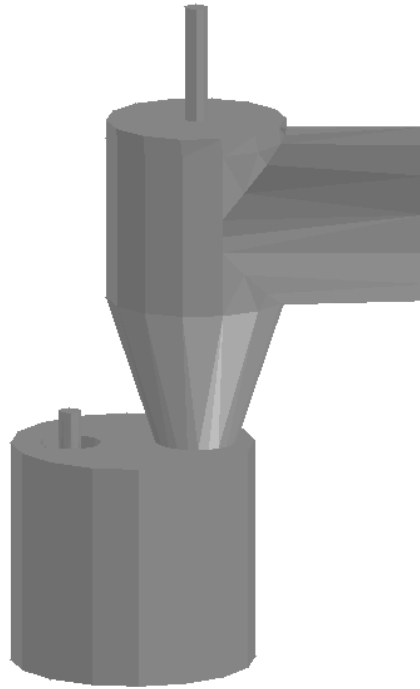
Transient - PH-2009 demonstration case

Following unsuccessful attempts using another mainstream CFD product, EA Technical Solutions Ltd approached CHAM for the purpose of obtaining a CFD code suitable for investigating the gas mixing processes within various air injector models. The problem specified below involves the transient purging of a hot gas chamber with cold gas from a pressurised chamber. In this case, there are pre-set inlet and exit valve positions with impermeable membranes. The flow field is stagnant initially, but the flow is initiated by the instantaneous removal of the two (purple) membranes.

The geometry of the air injector was generated by PTC's ProEngineer and exported as a 3D solid model in STL format – a format readily accepted by PHOENICS.



The requirement was to find the time taken for the cold air to just start to exit through the exhaust valve. Different model variations have the inlet valve moved into the neck to vary the cold flow direction.



Air Injector imported from CAD

CFD Model Description

Initial Conditions:

Hot Gas Chamber - Pressure 4 bar, Temperature 500K.

Cold Gas Chamber - Pressure 1 bar, Temperature 800K.

Stagnant flow in both chambers.

Conservation & Transport Equations:

Continuity, three momentum equations, static temperature, marker variable for cold-chamber gas, turbulent kinetic energy and its rate of dissipation.

Boundary conditions:

Adiabatic walls with empirical, equilibrium, log-law wall functions.

Fluid properties:

Working fluid is air.

Density: Ideal-gas law.

Specific heat: $C_p = 1064 \text{ J/kgK}$

Thermal conductivity: $k=0.0495 \text{ W/mK}$

Kinematic molecular viscosity:

$$\nu = -4.9468 \cdot 10^{-6} + 4.5839 \cdot 10^{-8} T + 8.0924 \cdot 10^{-11} T^2$$



Numerical Parameters:

PARSOL Cartesian cut-cell solver with residual cut-cell volumes of 5%

Mesh: 179 * 66* 123 = 1.453 million cells

Time Duration of Simulation: 2ms

Time Step: 5 μ s (400 uniform time steps)

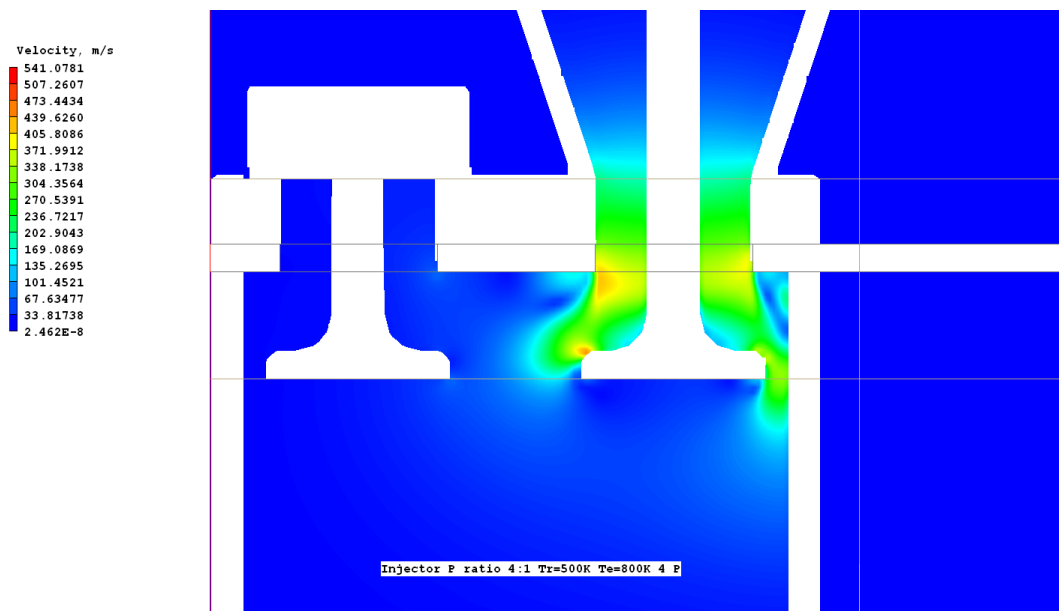
Typically 40 sweeps per time step

Note: As this was a demonstration case, there was no optimisation made in respect of mesh, time stepping, relaxation practices, and iteration numbers.

Version used: PHOENICS 2009 (64-bit Intel)

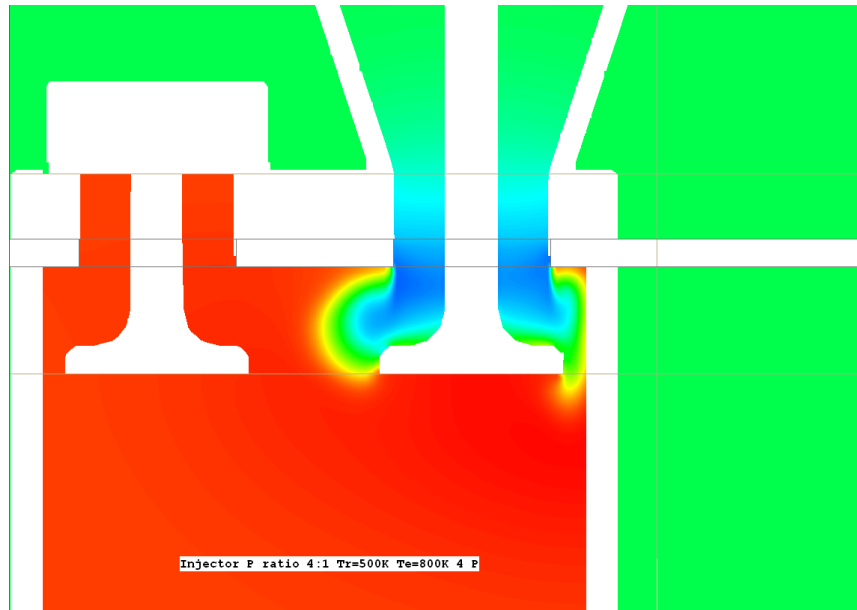
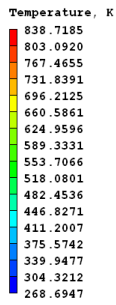
Elapsed run time: 78hrs Parallel with 4 processors.

Result Images

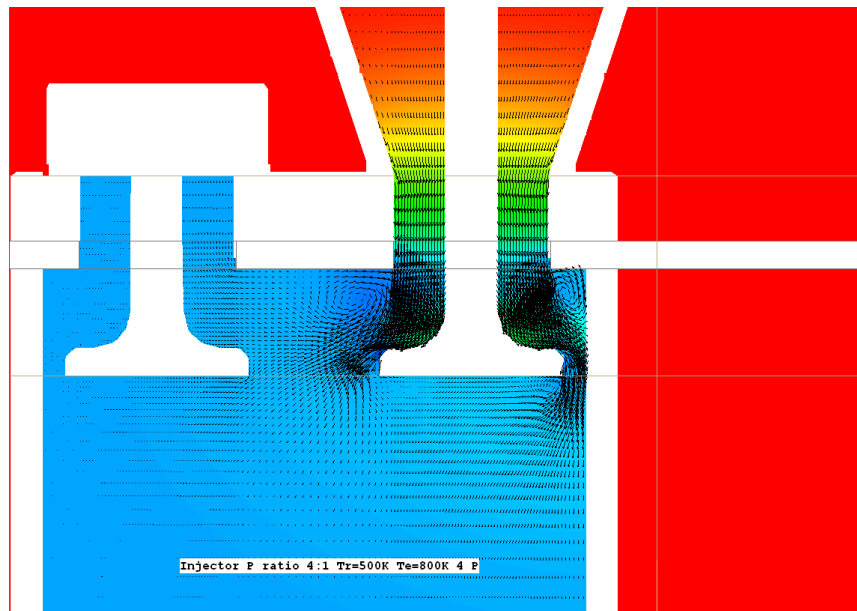
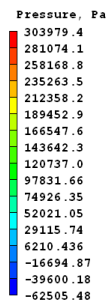


Velocity – Timestep 10

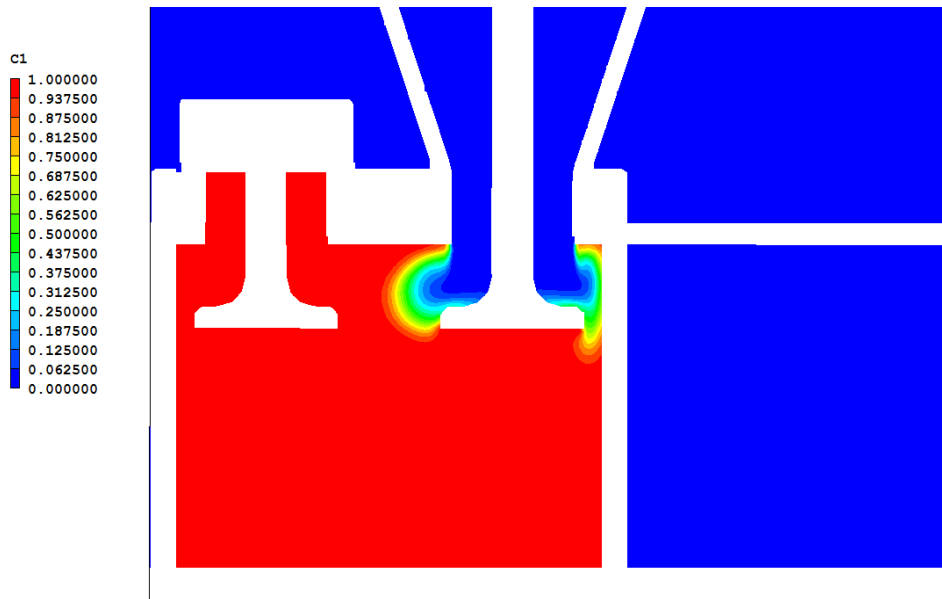
[Early in the process]



Temperature – Timestep 10



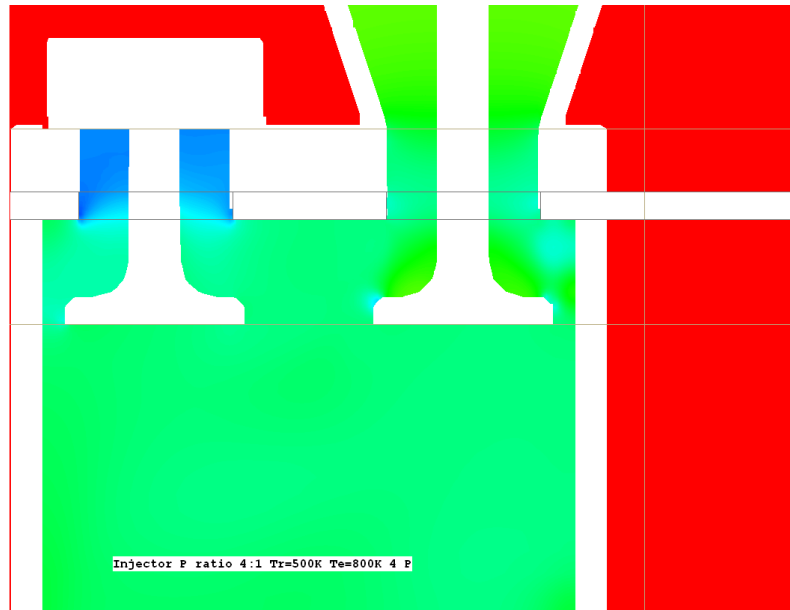
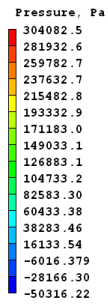
Pressure – Timestep 10 (+ velocity vectors)



Injector P ratio 4:1 Tr=500K Te=800K 4 P

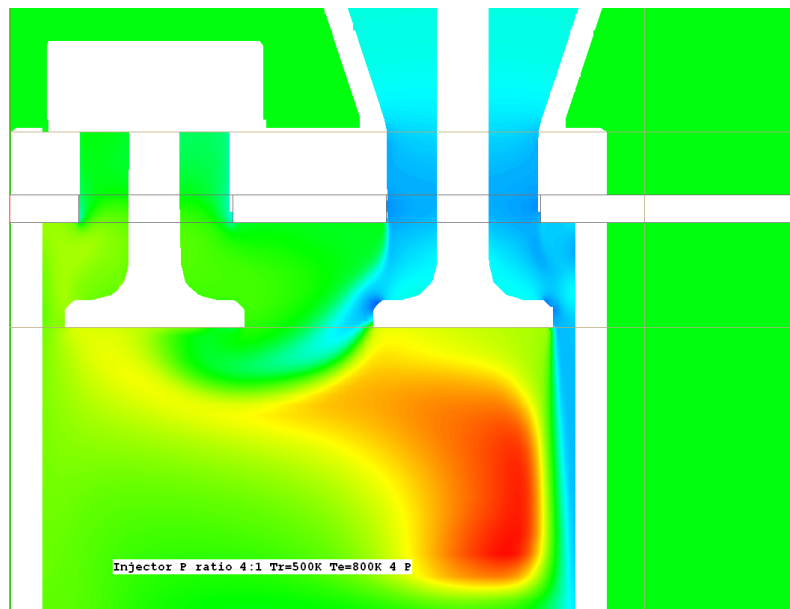
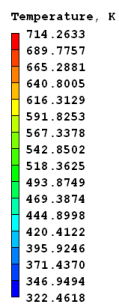
C1 (Hot gas marker) – Timestep 10

[Progression of cold gas flushing the hot]



Pressure – Timestep 220

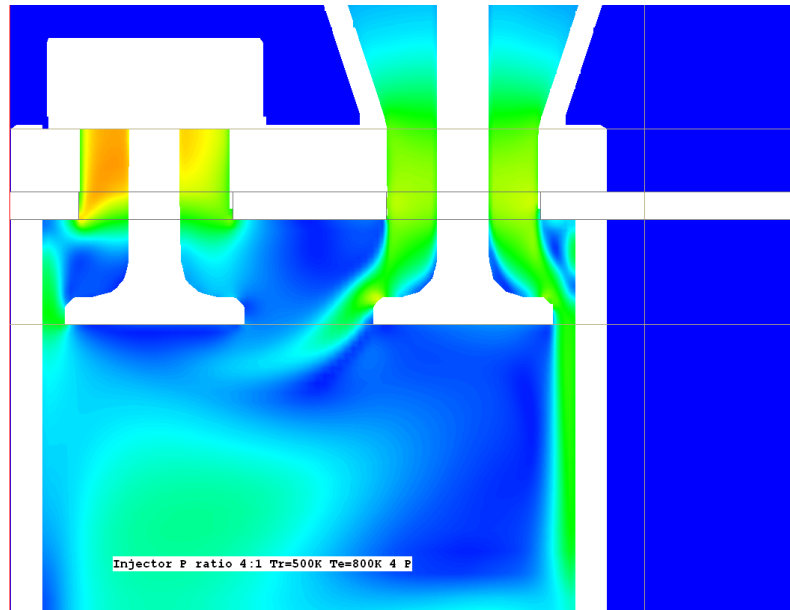
[Mid-way through the process]



Temperature – Timestep 220

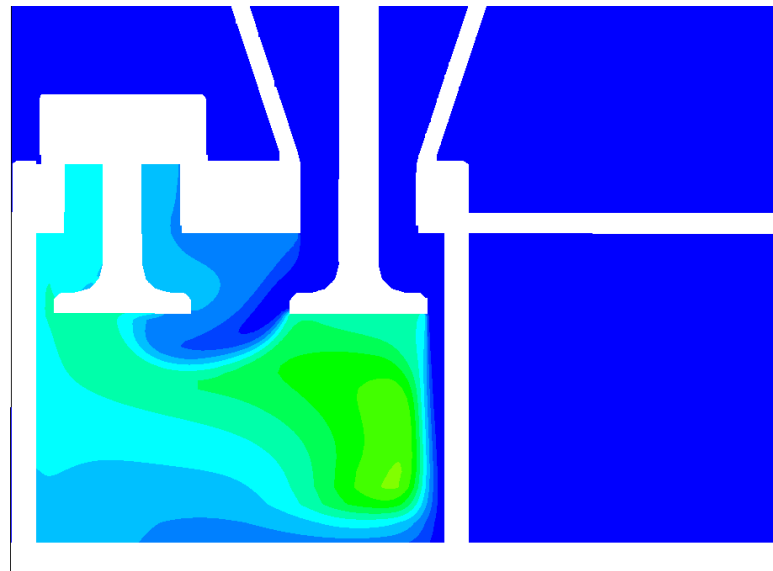


Velocity, m/s
483.1119
452.9174
422.7230
392.5284
362.3340
332.1395
301.9450
271.7505
241.5560
211.3615
181.1670
150.9725
120.7780
90.58349
60.38899
30.19450
1.100E-6



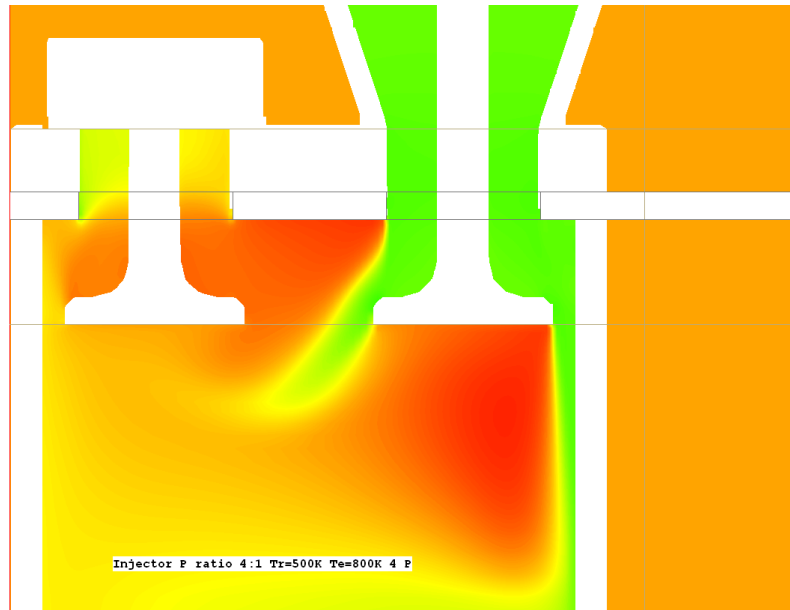
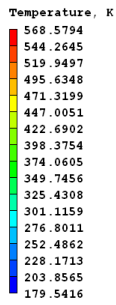
Velocity – Timestep 220

c1
1.000000
0.937500
0.875000
0.812500
0.750000
0.687500
0.625000
0.562500
0.500000
0.437500
0.375000
0.312500
0.250000
0.187500
0.125000
0.062500
0.000000



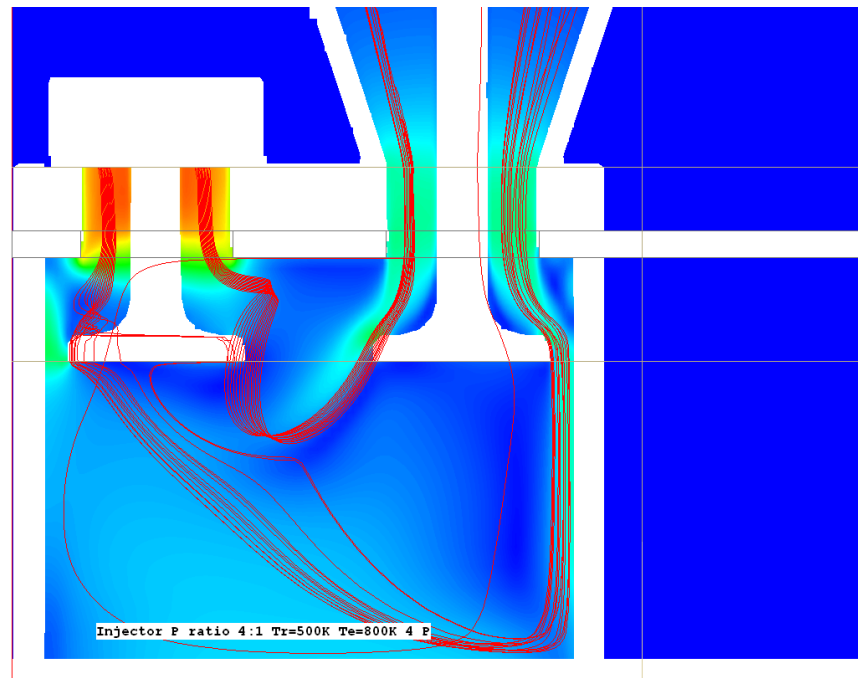
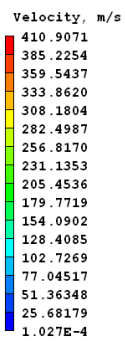
Injector P ratio 4:1 Tr=500K Te=800K 4 P

C1 (Hot gas marker) – Timestep 220

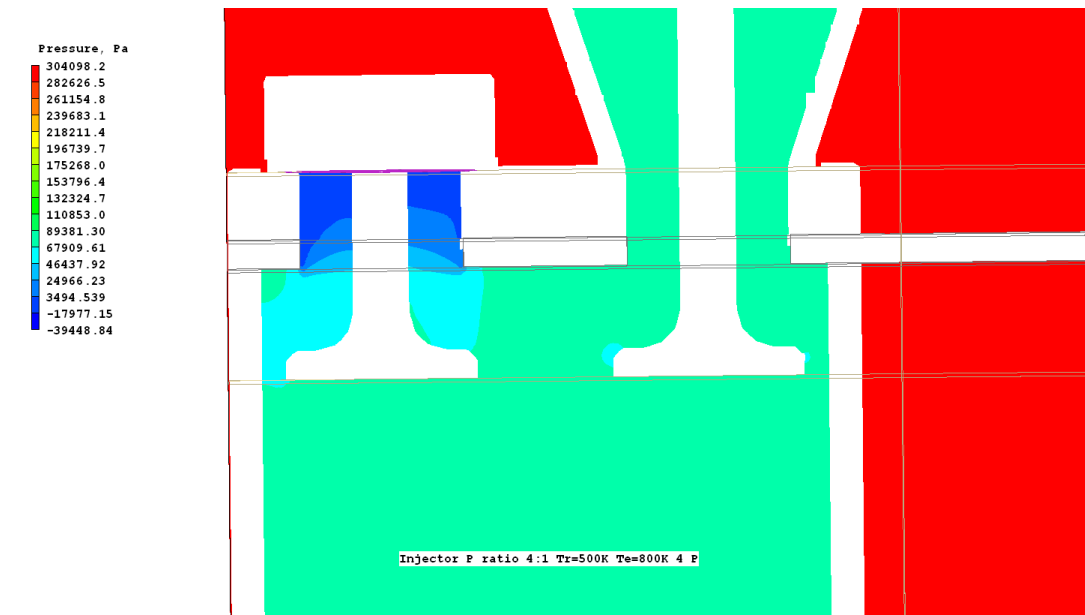


Temperature – Timestep 400

[Near-end of the process]



Velocity – Timestep 400 (+ streamlines)



Pressure – Timestep 400



C1 (Hot gas marker) – Timestep 345 (T400 plot unavailable)

Note: Whilst the scale used in the animated results (see below) remains constant, the scales used in some of the images shown above do vary.



Conclusion

Complex geometry and boundary conditions, involving both high pressure, temperature and velocity gradients, are characterized in this example. It has been demonstrated that PHOENICS can adequately capture the instantaneous removal of the 'idealised' separating membrane and the subsequent gas-mixing and exhaust process.

Diaphragm rupture is a phenomenon that attracts a high interest in the scientific world as it is the mean feature characterising shock tubes. These are widely employed when studying gas-phase combustion reactions or problems involving values of pressure and temperature that are not easily reproduced in a test rig. The main challenge for CFD codes in modelling this class of problems is the fast propagation of waves through the low-pressure zones.

Optimised results for this case could be obtained by localised refinement of the mesh where high- pressure ratios are present, adjustment of the time step, or greater attention to the relaxations factors. Such optimisation can lower the computational cost while achieving better accuracy.

A high fidelity model of the air injector would involve the movement of the valves, capabilities included in the PHOENICS package, as they open and close over time - an example of which can be found at: [www.cham.co.uk/DOCS/Polar PARSOL Demo cases.doc](http://www.cham.co.uk/DOCS/Polar_PARSOL_Demo_cases.doc)

Animated results

Temperature:	tstat.avi (2.98MB)
Pressure:	pstat.avi (3.04MB)
Velocity:	vect.avi (5.27MB)
Hot gas marker variable:	c1.avi (4.28MB)